渠務署及城市規劃委員會:

A/YL-KTN/1018 的渠務報告詳細

申請地點範圍有約 1,559.1 平方米,位於錦田北的鄉郊範圍。目前為露 天空間及建有臨時建築物。

申請地點附近有大量的臨時建築物及草地。現有水平為約+14.4 mPD (此水平已完成填土及平整)。

有一條自然溪流位於申請地點的東面,並計劃將場內水流引導到該溪 流。

申請範圍的東北面水平比申請地點高,有機會會有水流從這面流入。申 請範圍北外改有約 450mm 的渠道,因此沒有流水從其他方向流入申請地點。

申請地點的擬議佈局平面圖請參考 Appendix 2。

申請地點範圍有約1,559.1平方米,全部將以混凝土作表面,在申請地點外有約4,115.9平方米,大多為草地、道路及建築物。

擬議發展	
申請地點範圍 (約 m ²),全部已以混	1,559.1
凝土平整	
申請地點外集水區	
申請地點外北面集水區 (約 m ²),大	4,115.9
多為草地、道路及建築物,本報告將	
以約 93%混凝土作評估	

根據 STORMWATER DRAINAGE MANUAL (SDM) - Table 10 - Recommended Design Return

Periods based on Flood Levels

Intensively Used Agricultural Land	2-5 years
Village Drainage including Internal Drainage	10 years
System under a Polder Scheme	
Main Rural Catchment Drainage Channels	50 years
Urban Drainage Trunk Systems	200 years
Urban Drainage Branch Systems	50 years

本報告將使用 Main Rural Catchment Drainage Channels, 1 in 50 years return period 作評 估。

本渠道設計將參考由 貴署所編寫的 SDM 作基礎,以下為所採用的數據及計算方法。

 Intensity-Duration-Frequency Relationship - The Recommended Intensity-Duration-Frequency relationship is used to estimate the intensity of rainfall. It can be expressed by the following algebraic equation.

$$i = \frac{a}{(t_d + b)^c}$$

The site is located within the HKO Headquarters Rainfall Zone. Therefore, for 50 years return period, the following values are adopted.

а	=	451.3
b	=	2.46
с	=	0.337

2. The peak runoff is calculated by the Rational Method.

$$Q_p = 0.278 \ C \ i \ A$$

where	V	=	peak runoff in m ³ /s
	С	=	runoff coefficient (dimensionless)
	i	=	rainfall intensity in mm/hr
	А	=	catchment area in km ²

3. According to Section 7.5.2(b) of the Stormwater Drainage Manual (SDM), Fifth Edition January 2018

Surface Characteristics	Runoff coefficient, C
Asphalt	0.70-0.95
Concrete	0.80-0.95
Brick	0.70-0.85
Grassland (heavy soil)	
Flat	0.13-0.25
Steep	0.25-0.35
Grassland (sandy soil)	
Flat	0.05-0.15
Steep	0.15-0.20

The run-off coefficient (C) of surface runoff area taken as follows:

- Concrete Area C = 0.95
- Grassland (Heavy soil) with flat surface C = 0.25
- 4. Manning's Equation is used for calculation of velocity of flow inside the channels. It can be expressed by the following algebraic equation.

$$V = \frac{R^{1/6}}{n} \sqrt{RS_f}$$

where	V	=	Velocity of the pipe flow (m/s)
	S_f	=	Hydraulic gradient
	n	=	manning's coefficient
	R	=	Hydraulic radius (m)

5. Colebrook-White Equation is used for calculation of velocity of flow inside the pipes. It can be expressed by the following algebraic equation.

$$\overline{V} = -\sqrt{32gRS} \log\log\left(\frac{k_s}{14.8R} + \frac{1.255v}{R\sqrt{32gRS_f}}\right)$$

where V = Velocity of the pipe flow (m/s)

- S_f = Hydraulic gradient
- k_f = roughness value (m)
- v = kinematics viscosity of fluid
- D = pipe diameter (m)
- R = Hydraulic radius (m)

申請範圍主要平坦,並緩緩斜向東面,渠道設計請參考 Appendix 5。

渠道容量計算請參考 Appendix - Calculation。

根據本報告,本臨時發展不會對附近的渠道有重大影響。

二零二四年七月二十日

Check The Capacity of Existing Natural Stream

Manning Equation is used in hydraulic design and analysis. The cross-sectional mean velocity is given in the following expression:

$$V = \frac{R^{1/6}}{n} \sqrt{RS_f}$$

Where R = hydraulic (m) N = Manning coefficient (s/m1/3), refer Table 13 of SDM Sf = friction gradient (dimensionless)

Using Manning's Equation $V = R^{2/3*}S_f^{0.5}/n$

Where R	= A/P = 0.667 m	A = 4 m ² P = 6 m
n	= 0.05 s/m ^{1/3}	(Table 13 of Stormwater Drainage Manual)
Sf	= 0.245	
Therefor V	= 0.667 ^{2/3} *0.245 ^{0.5} /0 = 7.55 m/sec	0.05
Maximum Capacity (C	Qmax)	
	= V*A	
	= 30.2 m ³ /sec	
	> Q _{total}	*Allowed 10% for situation.

The Existing Natural Stream has enough capacity.

Appendix – Calculation

Capacity Flows Estimation for Propose Catchments and Drainage System with 50 Year Return Period

A1. Calculation of On-Site Runoff (After Development)

7% Grassland (Heavy soil) with flat surface + 93% 5,675 0.005675 3.52 96.7 4.58 4.58 451.3 2.46 0.337 234 0.9 0.0051075 0.332	Surface Type	Catchment Area (A), m ²	Catchment Area (A), km ²	Average slope (H), m/100m	Flow path length (L), m	Inlet time (t _o), min	Time of Concentration (t _c), min	Duration (t _d), min	a (50 year return period)	b (50 year return period)	c (50 year return period)	(i) mm/hr	Runoff coefficient (C)	C×A	Peak runoff (Q _p), m³/s
	(Heavy soil) with	5,675	0.005675	3.52	96.7	4.58	4.58	4.58	451.3	2.46	0.337	234	0.9	0.0051075	0.332

A2. Calculation of the Capacity of Proposed Drainage (After Development)

Channel Type	Width, m	Depth, m	Slope Leng	Slone	Slono	Slono	Length m	Length m	Manning's Roughness	Cross Section	Wetted	Hydraulic	Mean	Capacity	Catchment	Runoff, m3/s	% of capacity	Sufficient
channel Type	wiath, m	Deptil, III	Slope	Length, m	Coefficient	Area, m2	Perimeter, m	radius, m	Velocity, m/s	flow, m3/s	Served, km ²	Runon, m5/5	flow	Capacity (Y/N)				
Concrete Channel	0.45	0.45	0.005	203	0.015	0.26	1.157	0.225	1.74	0.453	0.005675	0.332	73%	Y				

*Allowed 10% for siltation

Note:

Runoff is calculated in accordance with DSD's "Stormwater Drainage Manual – Planning, Design and Management" (SDM), fifth edition, January 2018.

Equation used:
$$t_0 = \frac{0.14465L}{H^{0.2}A^{0.1}}$$
 $t_c = t_0 + t_f$ $i = \frac{a}{(t_d + b)^c}$ $Q_p = 0.278 \ C \ i \ A \quad V = \frac{R^{1/6}}{n} \sqrt{RS_f}$

B1. Calculation of the runoff of Existing Drainage System

Surface Type	Catchment Area (A), m ²	Catchment Area (A), km²	Average slope (H), m/100m	Flow path length (L), m	Inlet time (t₀), min	Time of Concentration (t _c), min	Duration (t _d), min	a (50 year return period)	b (50 year return period)	c (50 year return period)	(i) mm/hr	Runoff coefficient (C)	CxA	Peak runoff (Q _p), m³/s
15% Concrete + 85% Grassland (Heavy soil) with steep surface	545,522	0.545522	24.5	1,470	29.93	29.93	29.93	451.3	2.46	0.337	140	0.44	0.24003	9.34
	•		· · · · · ·	1			1	1	1	1	1	· · · · · ·	Total	9.34

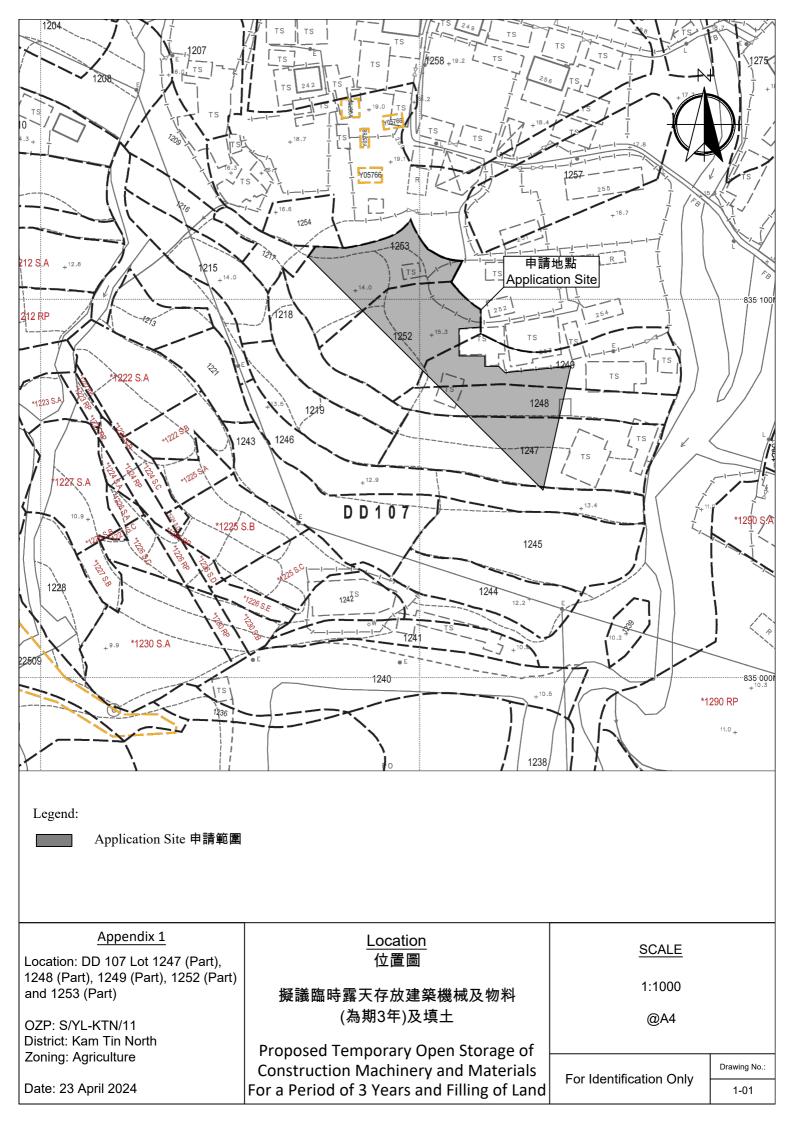
B2. Adequacy Check for Existing Drainage System

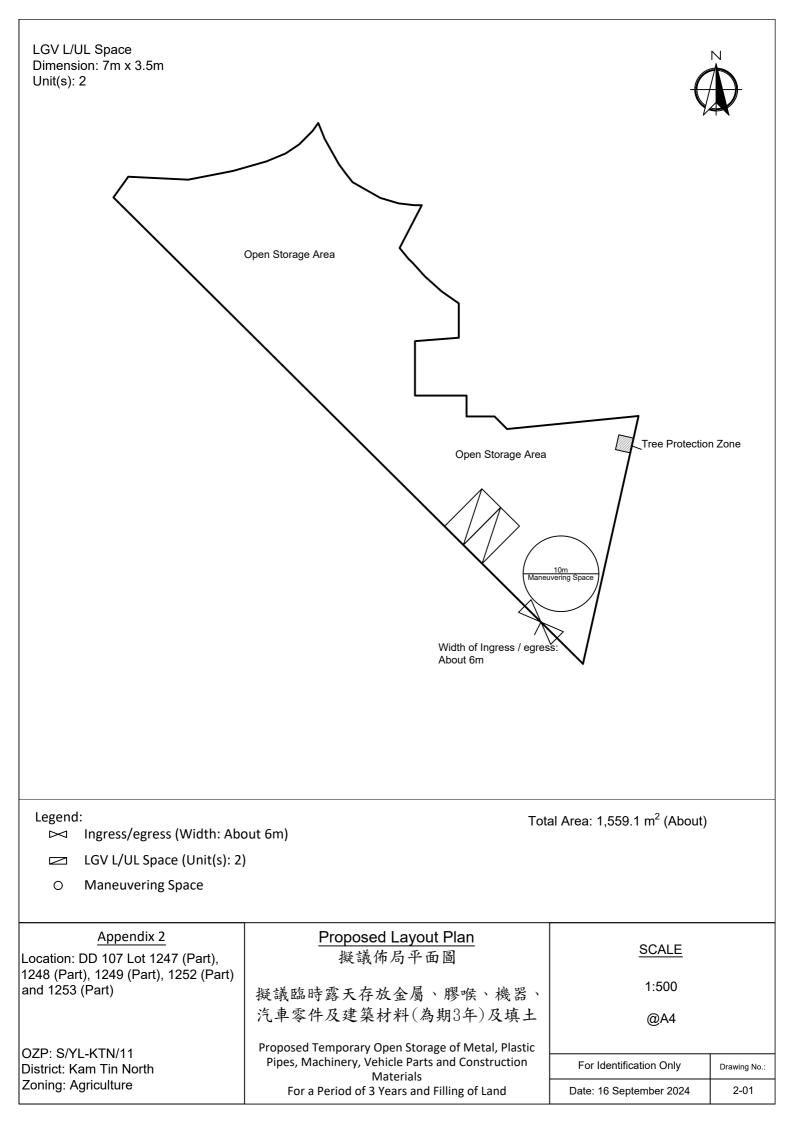
Channel Type	Width, m	Depth, m	Slope	Slope	length m	Length m	Length m	Length, m	length m	Length m	Longth m	Longth m	Longth m	Length m	Length m	Longth m	Manning's Roughness	Cross Section	Wetted	Hydraulic	Mean	Capacity	Catchment	Runoff, m3/s	% of capacity	Sufficient
Channel Type	width, in	Deptil, III	Siope	Length, m	Coefficient	Area, m2	Perimeter, m	radius, m	Velocity, m/s	flow, m3/s	Served, km ²	Kulloll, Ills/S	flow	Capacity (Y/N)												
Natural-Stream (7)	2	2	0.245	1,470	0.05	4	6	0.667	7.55	30.2	0.530231	9.34	31%	Y												

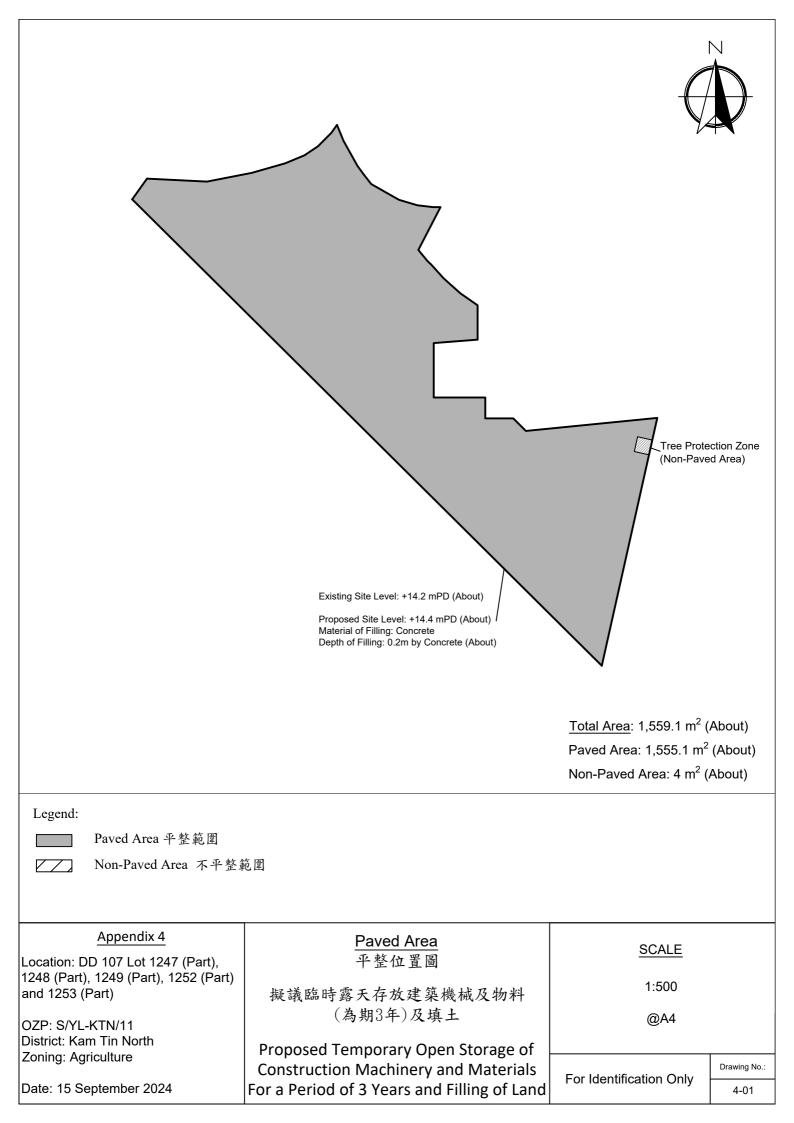
*Allowed 10% for siltation. For assessment purpose, assume width and depth of the channel is 2m.

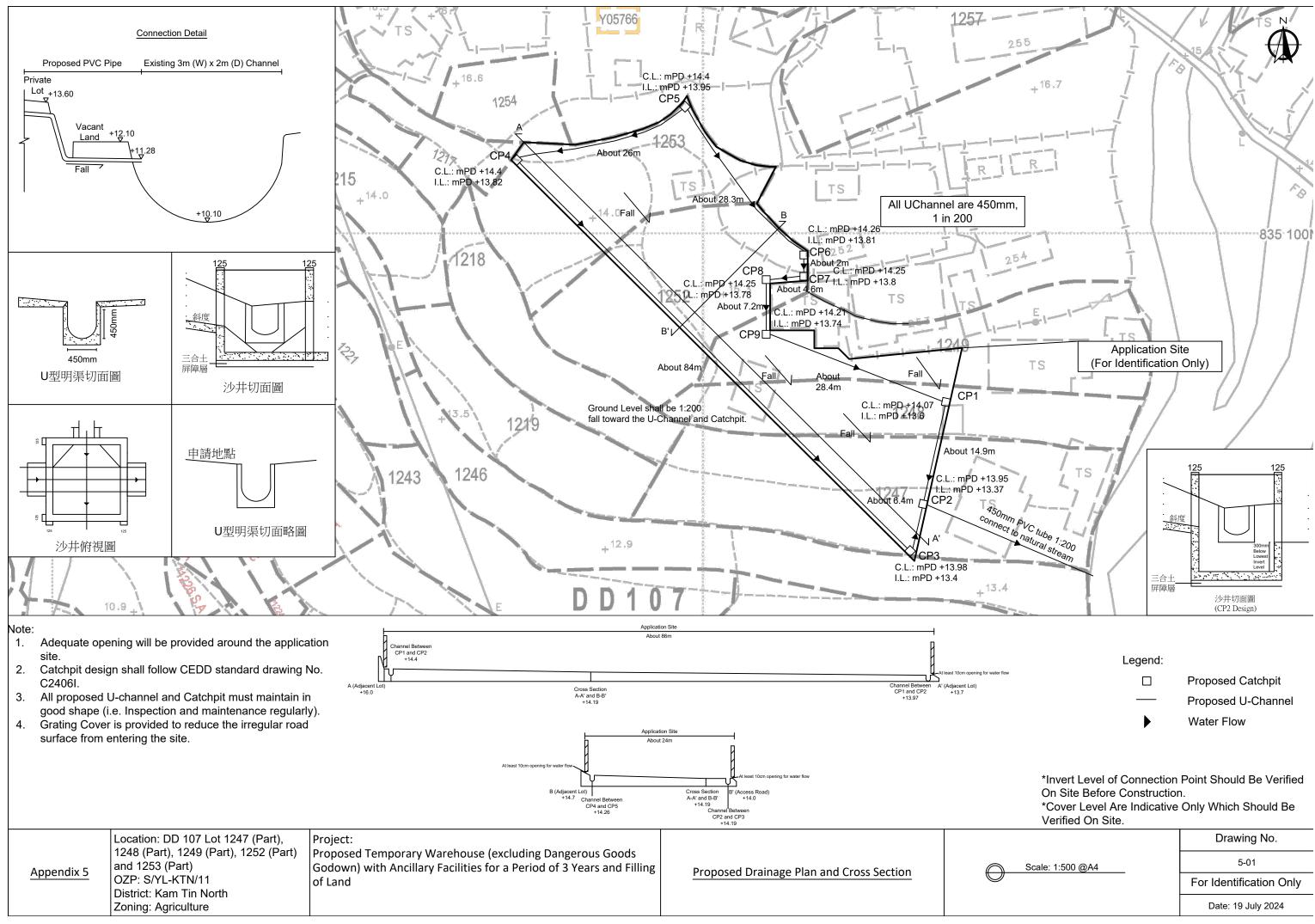
Total

0.332

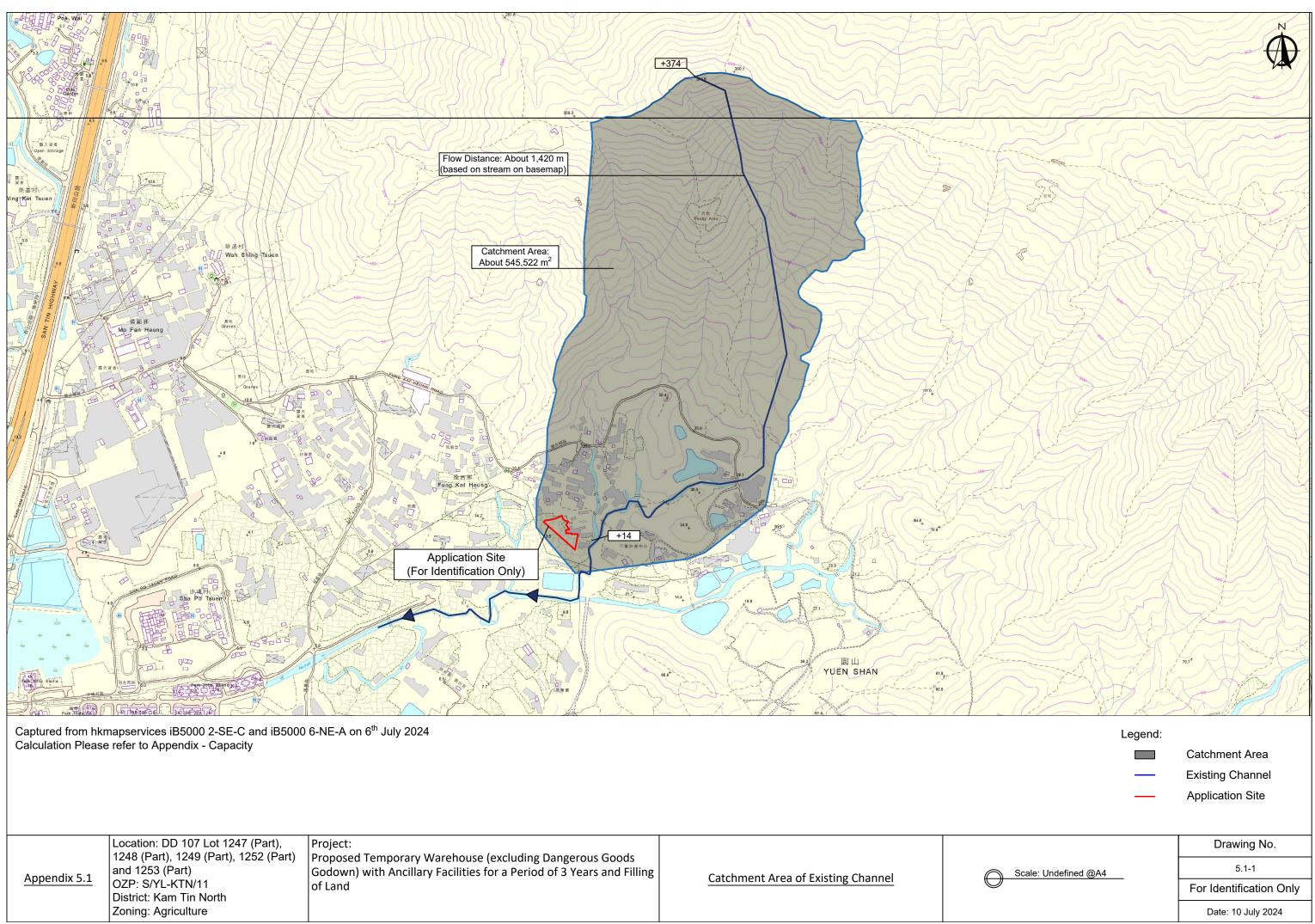




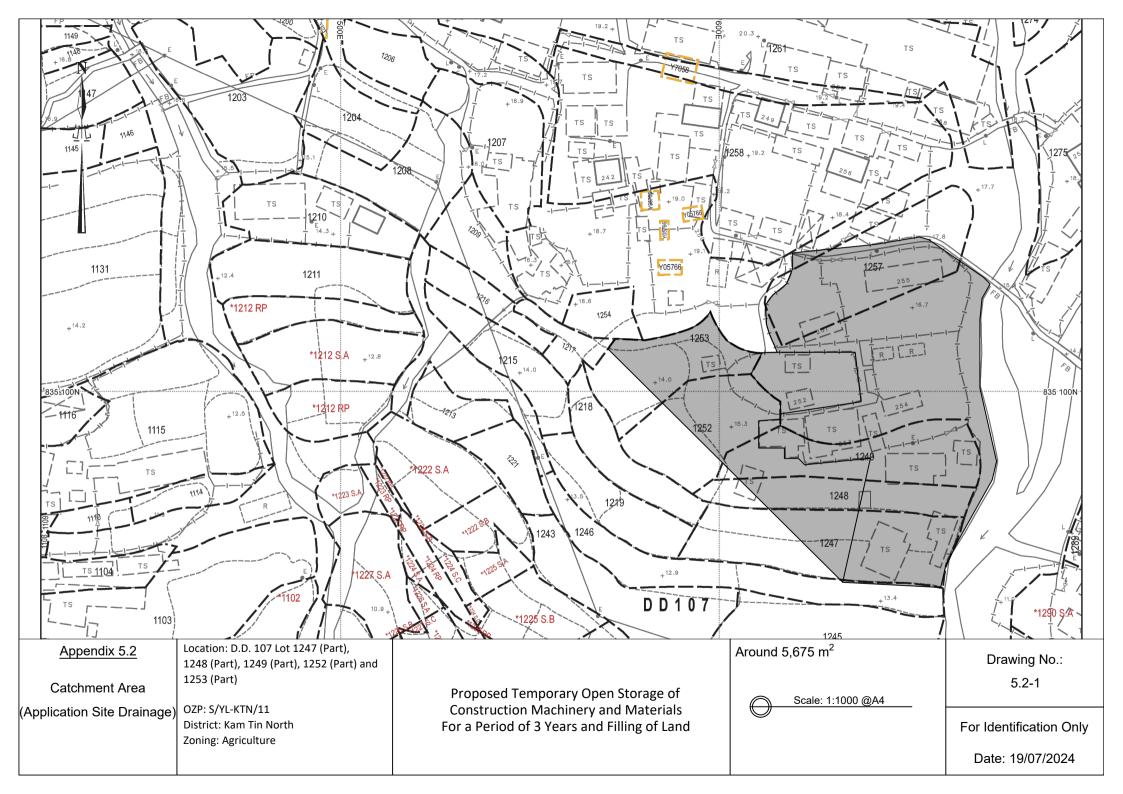


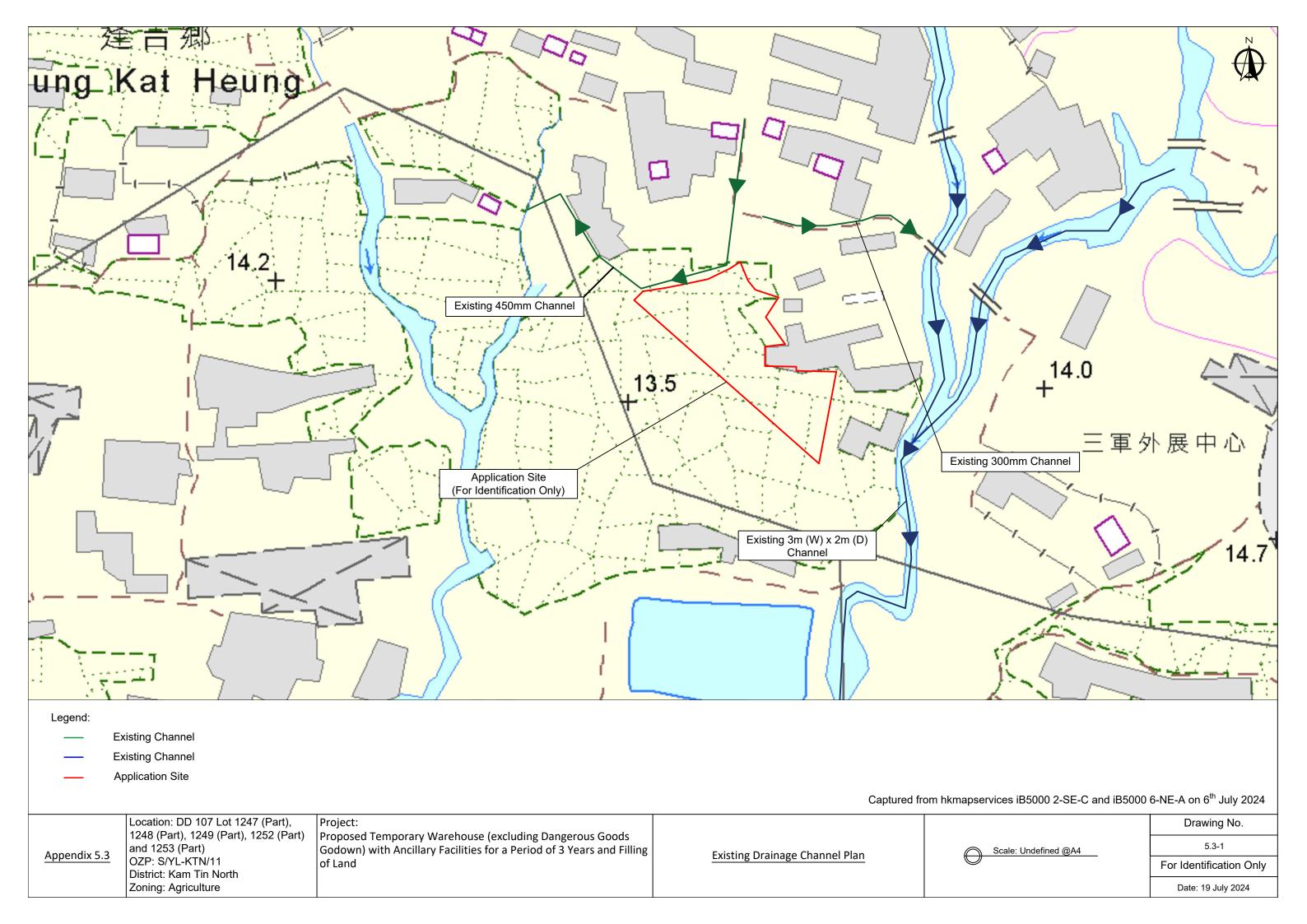


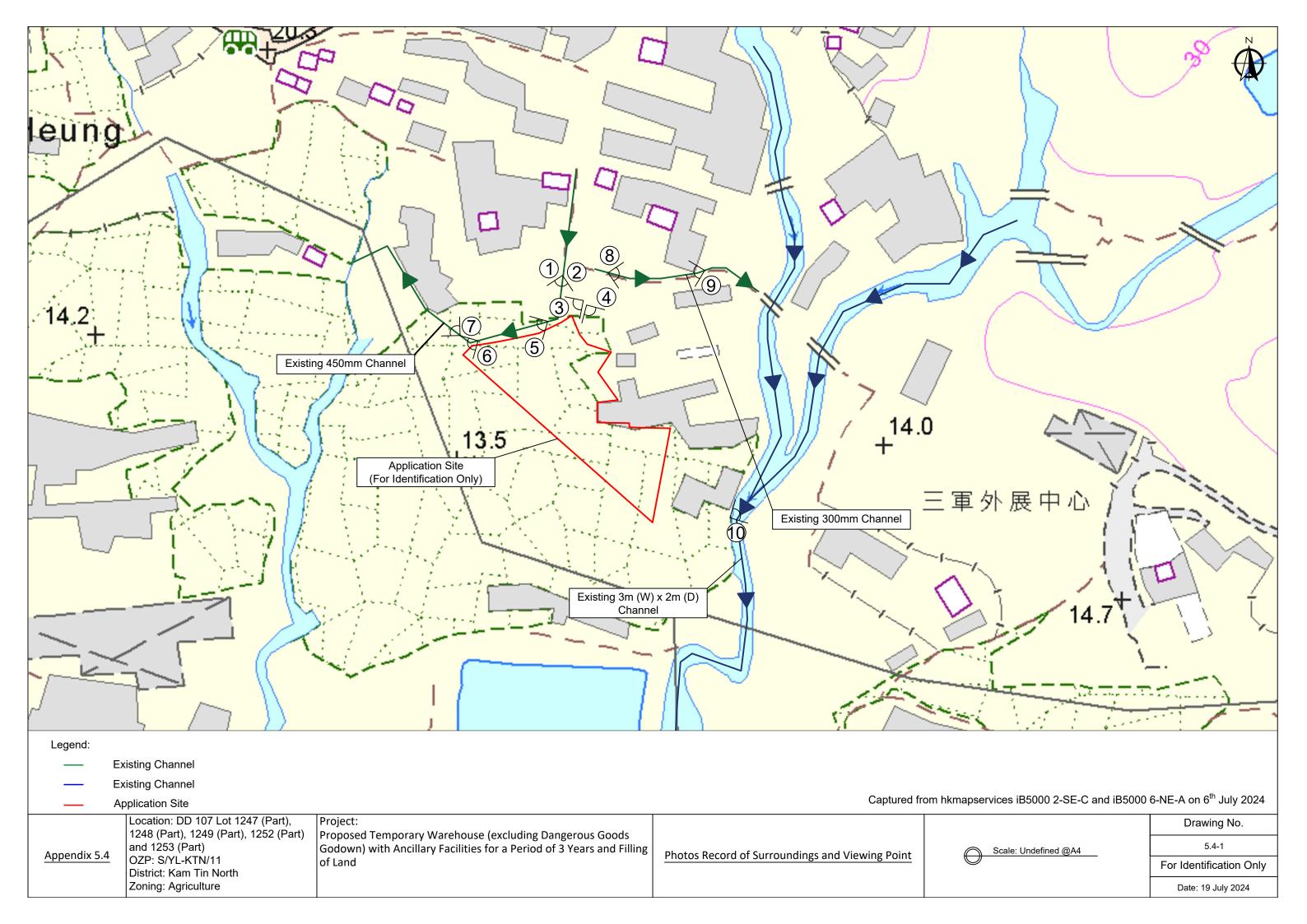
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	For Identification Only
	Date: 19 July 2024

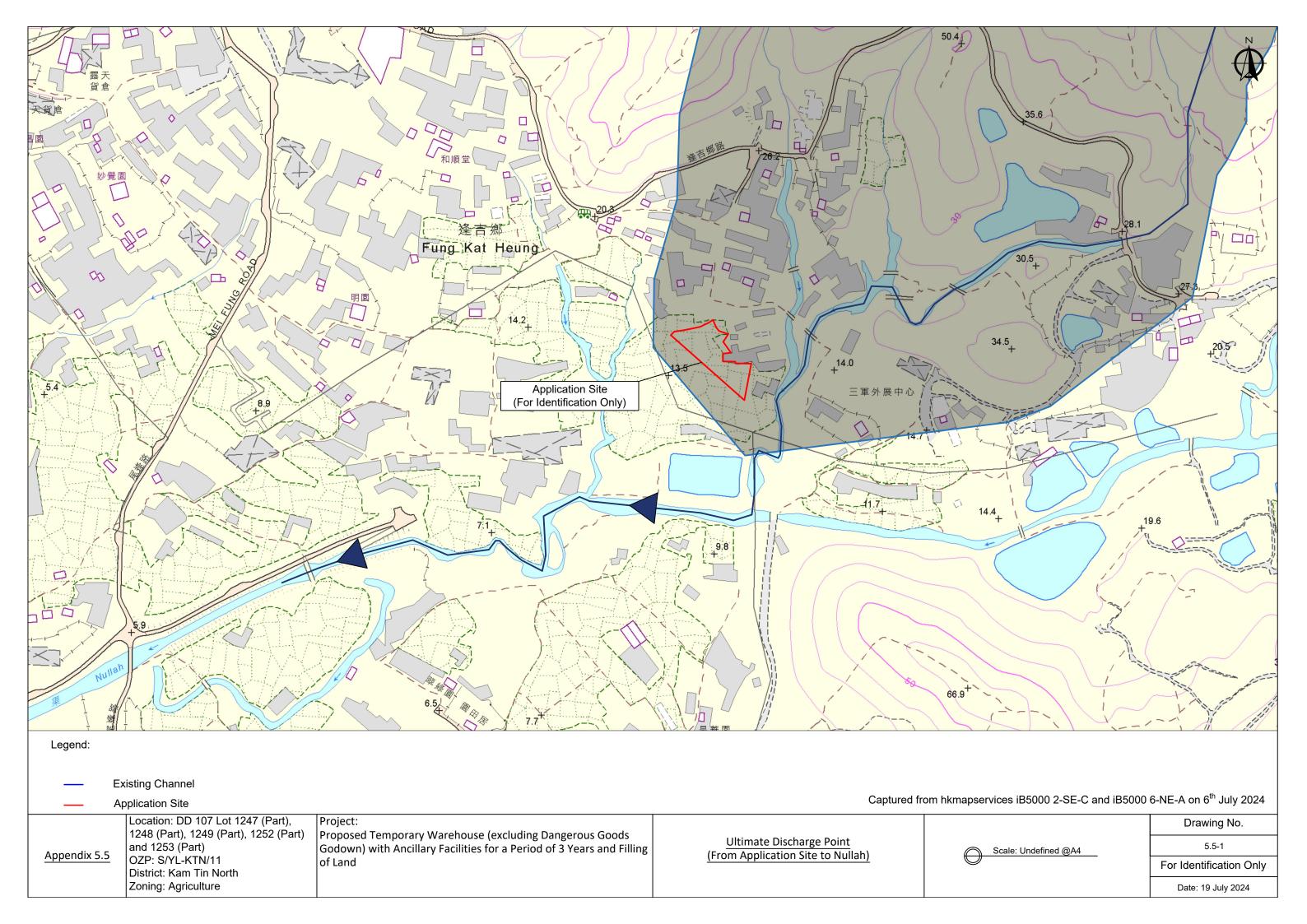


Appendix 5.1	and 1253 (Part) OZP: S/YL-KTN/11 District: Kam Tin North	Project: Proposed Temporary Warehouse (excluding Dangerous Goods Godown) with Ancillary Facilities for a Period of 3 Years and Filling of Land	Catchment Area of Existing Channel	
	Zoning: Agriculture			



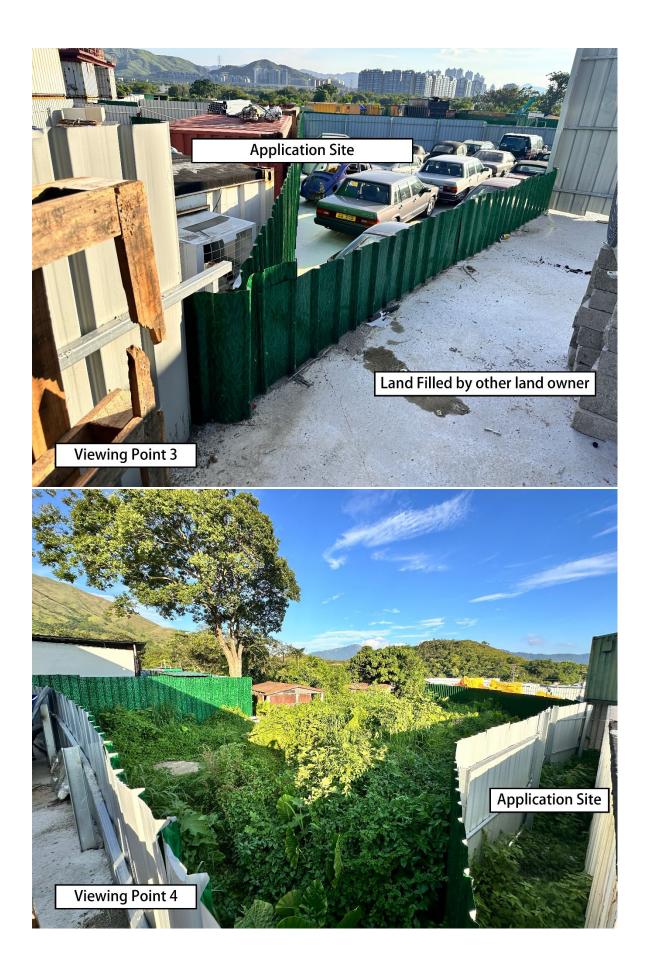






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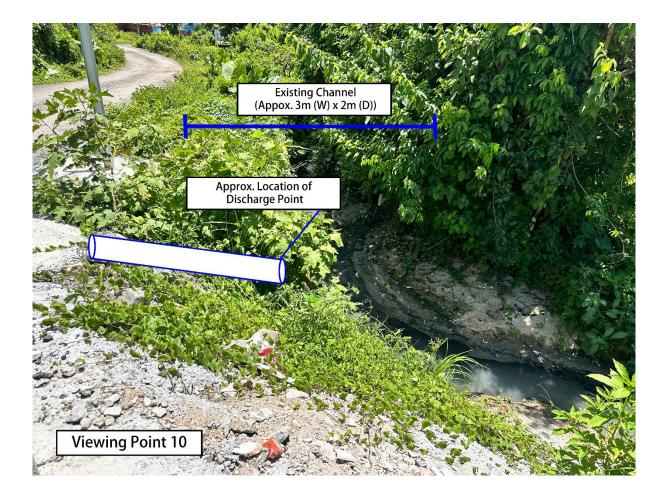


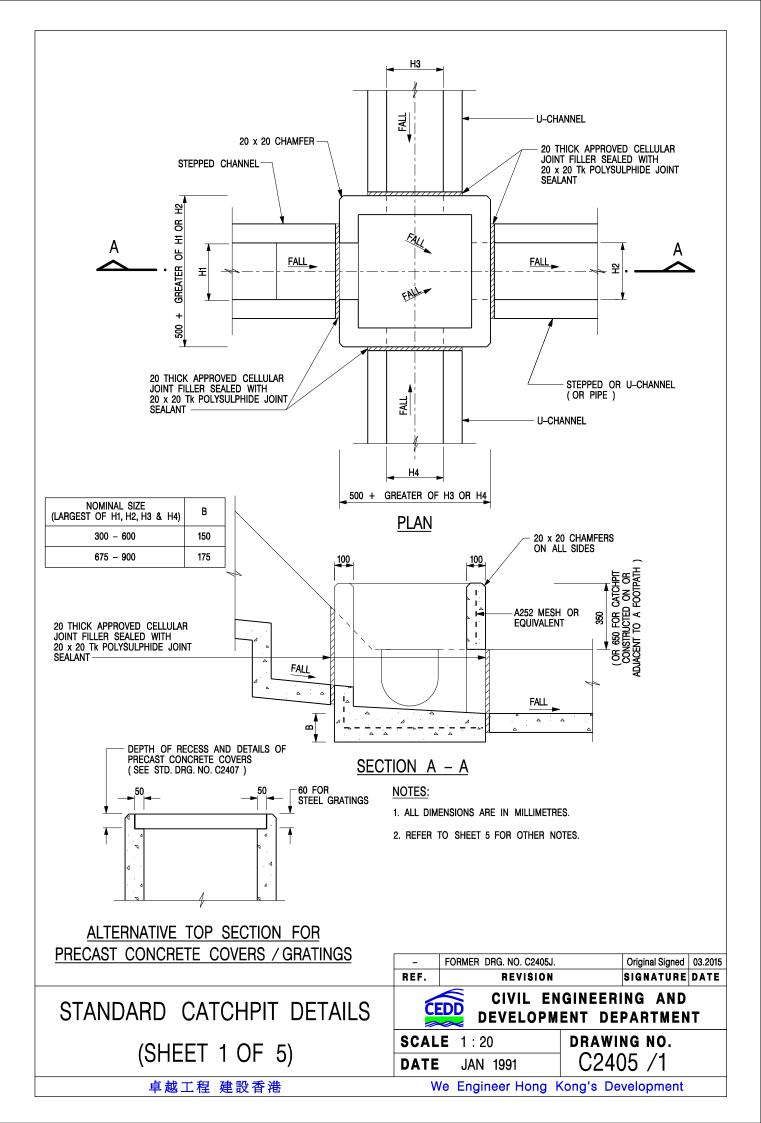


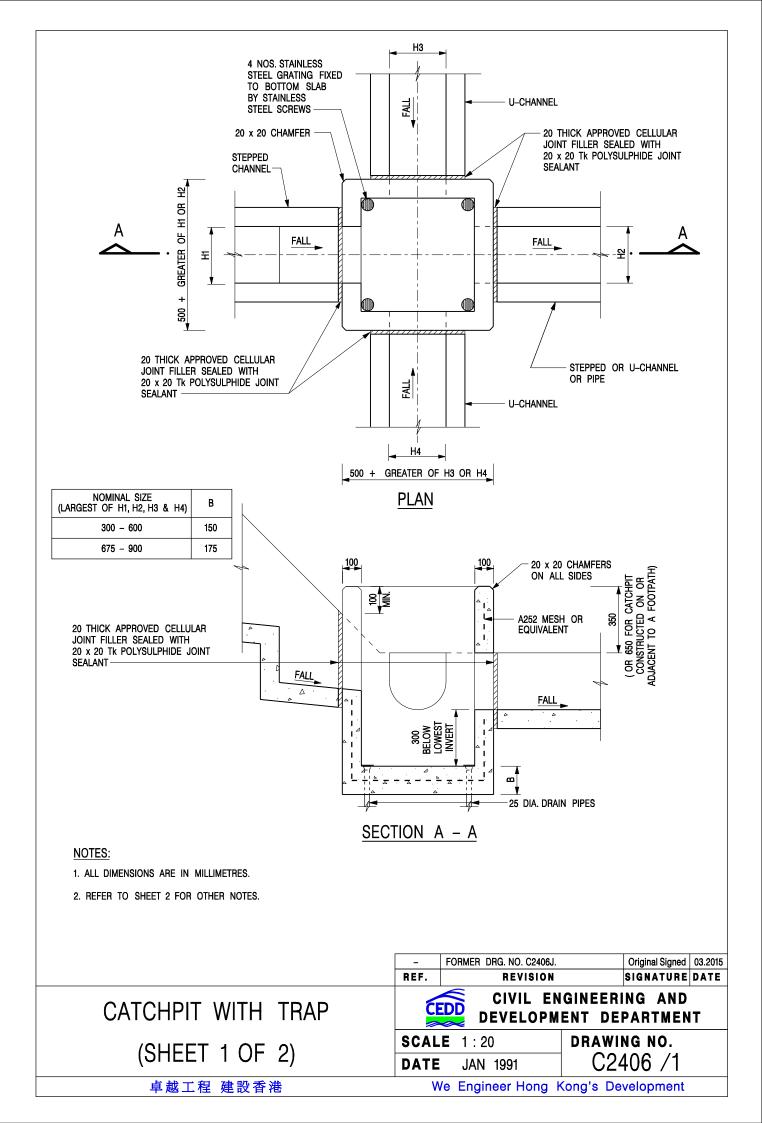


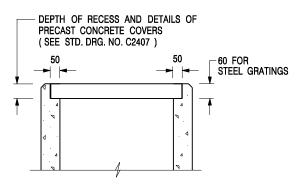










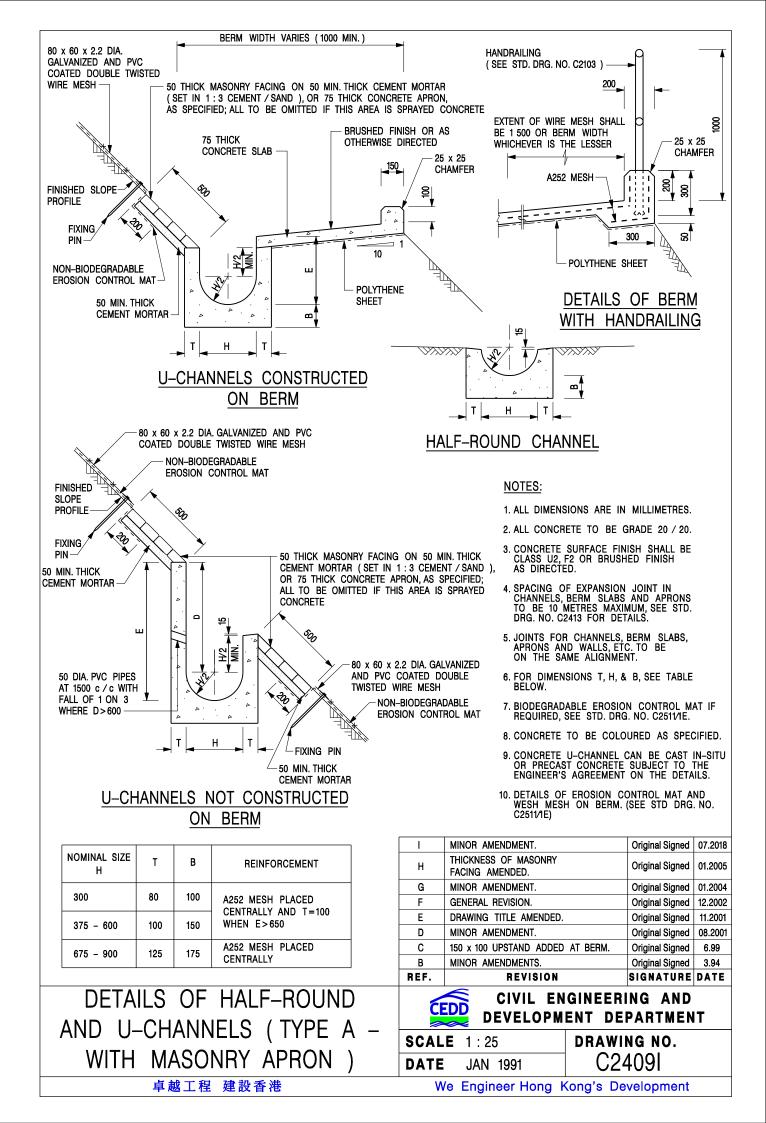


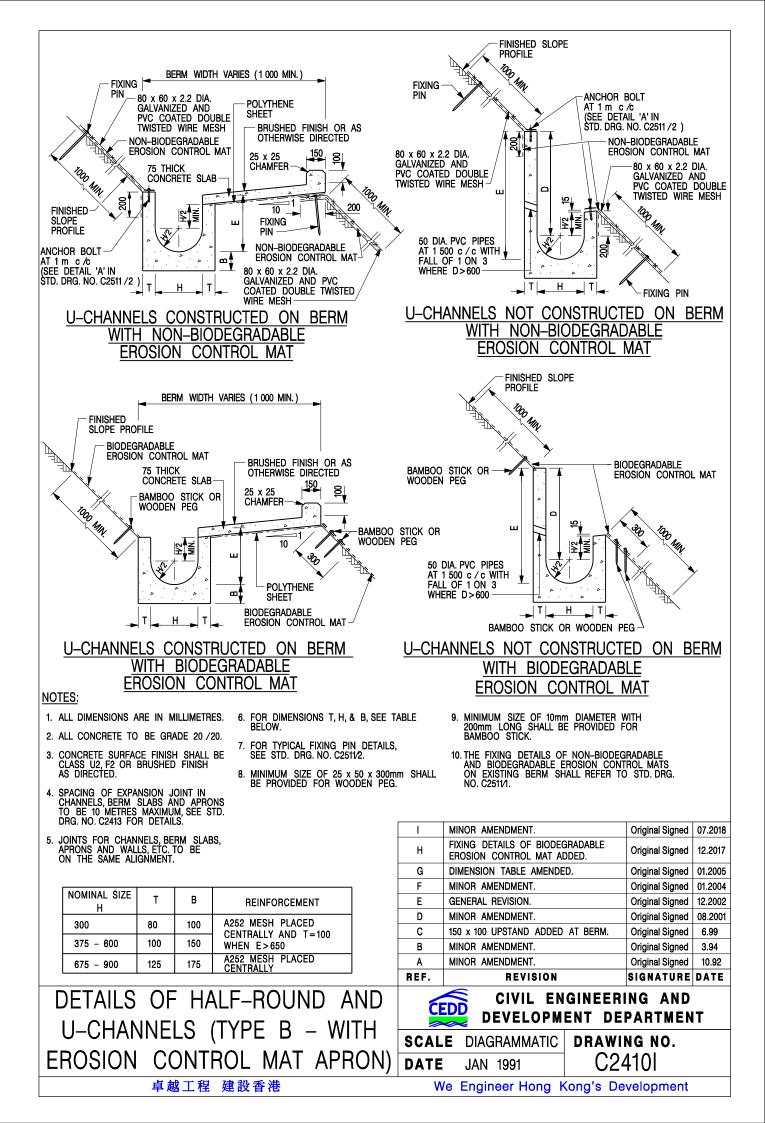
ALTERNATIVE TOP SECTION FOR PRECAST CONCRETE COVERS / GRATINGS

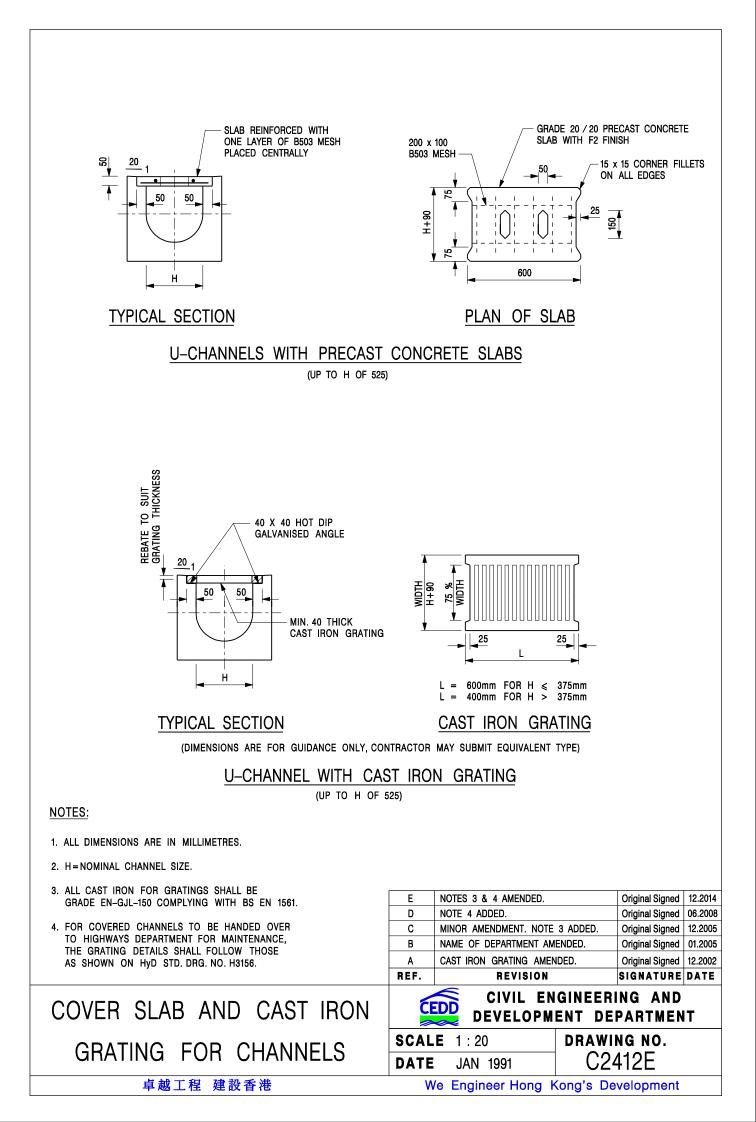
NOTES:

- 1. ALL DIMENSIONS ARE IN MILLIMETRES.
- 2. ALL CONCRETE SHALL BE GRADE 20 /20.
- 3. CONCRETE SURFACE FINISH SHALL BE CLASS U2 OR F2 AS APPROPRIATE.
- 4. FOR DETAILS OF JOINT, REFER TO STD. DRG. NO. C2413.
- 5. CONCRETE TO BE COLOURED AS SPECIFIED.
- UNLESS REQUESTED BY THE MAINTENANCE PARTY AND AS DIRECTED BY THE ENGINEER, CATCHPIT WITH TRAP IS NORMALLY NOT PREFERRED DUE TO PONDING PROBLEM.
- 7. UPON THE REQUEST FROM MAINTENANCE PARTY, DRAIN PIPES AT CATCHPIT BASE CAN BE USED BUT THIS IS FOR CATCHPITS LOCATED AT SLOPE TOE ONLY AND AS DIRECTED BY THE ENGINEER.
- FOR CATCHPITS CONSTRUCTED ON OR ADJACENT TO A FOOTPATH, STEEL GRATINGS (SEE DETAIL 'A' ON STD. DRG. NO. C2405 /2) OR CONCRETE COVERS (SEE STD. DRG. NO. C2407) SHALL BE PROVIDED AS DIRECTED BY THE ENGINEER.
- 9. IF INSTRUCTED BY THE ENGINEER, HANDRAILING (SEE DETAIL 'J' ON STD. DRG. NO. C2405 /5; EXCEPT ON THE UPSLOPE SIDE) IN LIEU OF STEEL GRATINGS OR CONCRETE COVERS CAN BE ACCEPTED AS AN ALTERNATIVE SAFETY MEASURE FOR CATCHPITS NOT ON A FOOTPATH NOR ADJACENT TO IT. TOP OF THE HANDRAILING SHALL BE 1 000 mm MIN. MEASURED FROM THE ADJACENT GROUND LEVEL.
- 10. MINIMUM INTERNAL CATCHPIT WIDTH SHALL BE 1 000 mm FOR CATCHPITS WITH A HEIGHT EXCEEDING 1 000 mm MEASURED FROM THE INVERT LEVEL TO THE ADJACENT GROUND LEVEL. AND, STEP IRONS (SEE DSD STD. DRG. NO. DS1043) AT 300 c¢ STAGGERED SHALL BE PROVIDED. THICKNESS OF CATCHPIT WALL FOR INSTALLATION OF STEP IRONS SHALL BE INCREASED TO 150 mm.
- 11. FOR RETROFITTING AN EXISTING CATCHPIT WITH STEEL GRATING, SEE DETAIL 'G' ON STD. DRG. NO. C2405 /4.
- 12. SUBJECT TO THE APPROVAL OF THE ENGINEER, OTHER MATERIALS CAN ALSO BE USED AS COVERS / GRATINGS.

	A	MINOR AMENDMENT.	Original Signed 04.2016
	-	FORMER DRG. NO. C2406J.	Original Signed 03.2015
	REF.	REVISION	SIGNATURE DATE
CATCHPIT WITH TRAP		. הוח	GINEERING AND Ent department
(SHEET 2 OF 2)	SCAL Date	E 1 : 20 JAN 1991	drawing no. C2406 /2A
卓越工程 建設香港	W	/e Engineer Hong K	(ong's Development







Return Period T (years)	2	5	10	20	50	100	200	500	1000
a	499.8	480.2	471.9	463.6	451.3	440.8	429.5	414.0	402.1
b	4.26	3.36	3.02	2.76	2.46	2.26	2.05	1.77	1.55
с	0.494	0.429	0.397	0.369	0.337	0.316	0.295	0.269	0.251

Table 3a – Storm Constants for Different Return Periods of HKO Headquarters

Table 3b - Storm Constants for Different Return Periods of Tai Mo Shan Area

Return Period T (years)	2	5	10	20	50	100	200
a	1743.9	2183.2	2251.3	2159.2	1740.1	1307.3	1005.0
b	22.12	27.12	27.46	25.79	19.78	12.85	7.01
с	0.694	0.682	0.661	0.633	0.570	0.501	0.434

Table 3c - Storm Constants for Different Return Periods of West Lantau Area

Return Period T (years)	2	5	10	20	50	100	200
a	2047.9	1994.1	1735.2	1445.6	1107.2	909.1	761.8
b	24.27	24.23	21.82	18.36	13.01	8.98	5.40
с	0.733	0.673	0.619	0.561	0.484	0.428	0.377

Table 3d - Storm Constants for Different Return Periods of North District Area

Return Period T (years)	2	5	10	20	50	100	200
a	1004.5	1112.2	1157.7	1178.6	1167.6	1131.2	1074.8
b	17.24	18.86	19.04	18.49	16.76	14.82	12.47
с	0.644	0.614	0.597	0.582	0.561	0.543	0.523

Table 13 - Values of n to be used with the Manning equation

Source: Brater, E.F. & King, H.W. (1976)

Surface	Best	Good	Fair	Bad
Uncoated cast-iron pipe	0.012	0.013	0.014	0.015
Coated cast-iron pipe	0.011	0.012*	0.013*	
Commercial wrought-iron pipe, black	0.012	0.013	0.014	0.015
Commercial wrought-iron pipe, galvanized	0.013	0.014	0.015	0.017
Smooth brass and glass pipe	0.009	0.010	0.011	0.013
Smooth lockbar and welded "OD" pipe	0.010	0.011*	0.013*	
Riveted and spiral steel pipe	0.013	0.015*	0.017^{*}	
Vitrified sewer pipe	0.010	0.013*	0.015	0.017
Common clay drainage tile	0.011	0.012*	0.014^{*}	0.017
Glazed brickwork	0.011	0.012	0.013*	0.015
Brick in cement mortar; brick sewers	0.012	0.013	0.015*	0.017
Neat cement surfaces	0.010	0.011	0.012	0.013
Cement mortar surfaces	0.011	0.012	0.013*	0.015
Concrete pipe	0.012	0.013	0.015^{*}	0.016
Wood stave pipe	0.010	0.011	0.012	0.013
Plank flumes - Planed	0.010	0.012*	0.013	0.014
- Unplaned	0.011	0.013*	0.014	0.015
- With battens	0.012	0.015*	0.016	
Concrete-lined channels	0.012	0.014*	0.016*	0.018
Cement-rubble surface	0.017	0.020	0.025	0.030
Dry-rubble surface	0.025	0.030	0.033	0.035
Dressed-ashlar surface	0.013	0.014	0.015	0.017
Semicircular metal flumes, smooth	0.011	0.012	0.013	0.015
Semicircular metal flumes, corrugated	0.0225	0.025	0.0275	0.030
Canals and ditches				
1. Earth, straight and uniform	0.017	0.020	0.0225*	0.025
2. Rock cuts, smooth and uniform	0.025	0.030	0.033*	0.035
3. Rock cuts, jagged and irregular	0.035	0.040	0.045	
4. Winding sluggish canals	0.0225	0.025*	0.0275	0.030
5. Dredged-earth channels	0.025	0.0275*	0.030	0.033
6. Canals with rough stony beds, weeds on earth banks	0.025	0.030	0.035*	0.040
7. Earth bottom, rubble sides	0.028	0.030*	0.033*	0.035
Natural-stream channels				
1. Clean, straight bank, full stage, no rifts or deep pools	0.025	0.0275	0.030	0.033
2. Same as (1) but some weeds and stones	0.030	0.033	0.035	0.040
3. Winding some pools and shoals, clean	0.033	0.035	0.040	0.045
4. Same as (3), lower stages, more ineffective slope and sections	0.040	0.045	0.050	0.055

Table 13 (Cont'd)

Surface	Best	Good	Fair	Bad
5. Same as (3) some weeds and stones	0.035	0.040	0.045	0.050
6. Same as (4) stony sections	0.045	0.050	0.055	0.060
 Sluggish river reach, rather weedy or with very deep pools 	0.050	0.060	0.070	0.080
8. Very weedy reaches	0.075	0.100	0.125	0.150

Notes: *Values commonly used for design.